# Unstructured mesh adaptation applied to CFD simulation.

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### Guideline

#### Introduction

Useful tools for mesh adaptation

Local remeshing

Generation of a computational mesh from an implicitly defined domain

Anisotropic mesh adaptation for immersed boundary method

# Mesh adaptation applications







# MMG platform: overview

- **MMG2D** : 2d meshing/remeshing
- **MMGS** : surfacic remeshing
- **MMG3D** : 3d remeshing

#### Developped by

• C. Dobrzynski (Bordeaux), C. Dapopny (Grenoble), P. Frey (Paris), A. Froehly (Bordeaux)

• Distribution: https://github.com/MmgTools/mmg

# Guideline

#### Introduction

#### Useful tools for mesh adaptation Drive the mesh process Evaluate a mesh

#### Local remeshing

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# Drive the mesh process

#### Generate a mesh suitable to numerical simulation



Uniform mesh

Non-uniform mesh

Non-uniform mesh

- Isotropic mesh : prescribed edge sizes
- At each point, give the prescribed sizes

# Drive the mesh process

#### Adapt the mesh to the numerical solution



- According to an error estimator, prescribe a size map
- Anisotropic case: sizes + directions

Mesh adaptation background: metric specification

Metric definition

 $d \times d$  symetric positive definite matrix:

$$M = \mathcal{R} \Lambda \mathcal{R}^{-1}$$

Edges orientation:  $\mathcal{R} = (\vec{v_1} \ \vec{v_2} \ \vec{v_3})$ 

Sizes prescription:  $\Lambda = diag(\lambda_1, \lambda_2, \lambda_3)$ 

Isotropic case

- $\lambda_1 = \lambda_2 = \lambda_3$
- ellipsoide  $\Rightarrow$  sphere



Ex: size prescription = 0.1

$$M = \left(\begin{array}{rrrr} 100 & 0 & 0\\ 0 & 100 & 0\\ 0 & 0 & 100 \end{array}\right)$$

#### Anisotropic metric example

$$M = \left(\begin{array}{rrrr} 100 & 0 & 0\\ 0 & 10 & 0\\ 0 & 0 & 10 \end{array}\right)$$



# Anisotropic metric example

Rotation of  $\frac{\pi}{4}$ :

$$M = \left(\begin{array}{rrrr} 55 & 0 & -45\\ 0 & 10 & 0\\ 0 & 0 & 45 \end{array}\right)$$





# Mesh adaptation background

• Length definition for an edge e:

$$l_M(e) = \int_0^1 \sqrt{e^t M(t)e} \, dt$$

• Metric intersection:

$$\mathcal{M} = \mathcal{M}_1 \cap \mathcal{M}_2$$



• Metric interpolation:  

$$\mathcal{M}(P) = \left(t \,\mathcal{M}(A)^{-\frac{1}{k}} + (1-t) \,\mathcal{M}(B)^{-\frac{1}{k}}\right)^{-k}$$

#### Error estimators examples

#### Isotropic

- Have a sensor (based on gradient variations of a quantity, hessian variations...)
- <sup>2</sup> Impose cell size or divide cell size in 2 if needed

#### Anisotropic

Interpolation error majoration on an element  $K^{1}$ :

$$\| u - \Pi_h u \|_{\infty, K} \leq \frac{9}{32} \max_{e \in E_K} \langle \vec{e}, \mathcal{M}(K) \vec{e} \rangle,$$

where  $\mathcal{M}(K)$  computed with the Hessian of u and  $\vec{e}$  an edge.

<sup>&</sup>lt;sup>1</sup>P. Frey and al., Comput. Methods Appl. Mech. Engrg., Vol. 194, Issues 48-49, 2005

### Guideline

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Geometric mesh Volumic remeshing Coupling surface/volume mesh generation

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# Local remeshing

#### Principles

- input : a mesh + (not mandatory) a size map
- modify iteratively the mesh

#### 2 main requirements

- well describe the underlying geometry
- be in agreement with the user-defined size map

#### Advantages

- only one mesh in memory,
- mesh always valid,
- in mesh adaptation process, very quick process.

# Control the underlying geometry

#### Principles

- input : a triangulated surface (no CAD)
- approximate the underlying geometry
- modify the mesh to control the geometric approximation

#### Tools

- surface models based on Bézier surface
- Hausdorff distance evaluation

#### Surface model: cubic surface



Parametric Bézier cubic surface  $b_{i,j,k}$  control points

#### Surface model: cubic surface



- 3-order Bézier surface
- $\forall (u,v) \in \hat{T},$

$$\sigma(u,v) = \sum_{i,j\in 0..3} \frac{3!}{i!j!k!} (1-u-v)^i u^j v^{1-i-j} b_{i,j,k}$$

# Surface model: control points

Triangle vertex (interpolate by the Bézier surface)  $a0 = b_{3,0,0}$   $a1 = b_{0,3,0}$   $a2 = b_{0,0,3}$ 

#### Edge vertex

- $T_{a_i}$ : tangent plane at vertex  $a_i$  defined by  $\vec{n}_i$  and  $a_i$ 
  - Hypothesis
    - **1** Tangents at  $a_i$  are onto  $T_{a_i}$
    - 2 Edges are curves with constant speed
  - Example for  $b_{2,1,0}$

• projection of 
$$a_1$$
 onto  $T_{a_0}$ 

$$a_0 \vec{b_{2,1,0}} = \frac{1}{3} a_0 \vec{a}_1$$

#### Last control point

• Such as if a quadratic surface exists, it coincides

#### Surface model

- Geometric elements identification (corners, edges...)
- Normal computation on each vertex P of the discrete surface

$$n(P) = \frac{\sum_{T \supset P} \alpha_T \times n_T}{||\sum_{T \supset P} \alpha_T \times n_T||} \text{ avec } \sum_{T \supset P} \alpha_T = 1$$

• Construction of a local geometry :

- 3-order Bézier surface
- $\forall (u,v) \in \hat{T},$

$$\sigma(u,v) = \sum_{i,j \in 0..3} \frac{3!}{i!j!k!} (1-u-v)^i u^j v^{1-i-j} b_{i,j,k}$$

# Geometric mesh algorithm

#### Main steps

- Geometric elements identification (corners, edges...)
- Construction of a local geometry
- Evaluation of the Haussdorff distance
- Nodes insertions/deletions to control the geometry
- Nodes relocations/edge swaps to improve the triangle quality

#### Surfacic node relocation



Point relocation

# Volumic remeshing

#### Principles

- drive by a user-defined size map
- no geometric constraints

#### Tools

- Nodes insertions
- Nodes deletions
- Edge swaps
- Nodes relocation

#### Node insertion by pattern



Point insertion by pattern.

• Delaunay measurement:

$$\alpha(K,P) = \frac{d(P,O_K)}{r_K}$$

• Cavity characterization:

$$K \in \mathcal{C}_P \text{ iff } \alpha(K, P) \leq 1.$$



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• Anisotropic extension:

$$\alpha(K,P)_{\mathcal{M}} = \frac{\ell_{\mathcal{M}}(P,O_K)}{r_K}$$

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# Node suppression

• Transform edge *AB* into vertex *C*. Three possibilities:

- Apply this operator if:
  - $\bullet$  all tetra containing C are valid (positive volume and admissible quality)
  - 2 new configuration has no big edges.

# Edge swap



Edge swap

#### Node relocation

- Find a new position for P such as:
  - all tet containing  $P^\prime$  have a better quality as the worst containing P
  - all edges from P' have an admissible lenght
- Optimal position:

For all tet *i* in the ball of *P*, the optimal position  $P_i^{opt}$  is:

$$P_i^{opt} = \frac{1}{3} \sum_{j=1}^{3} \left( P + \frac{\overrightarrow{PP_j}}{l(PP_j)} \right) \tag{1}$$

P' is found *via* a relaxation method as the barycenter of all the computed  $P_i^{opt}$ :

$$P' = (1 - \omega)P + \omega(\frac{1}{n_b} \sum_{i=1,\dots,n_b} P_i^{opt}).$$
 (2)

where  $\omega$  is the relaxation parameter (between 0 et 1).

# General algorithm

- mesh surface analysis
- 2 geometric remeshing (control of the Hausdorff distance)

- **3** Edge length analysis (both internal and surfacic)
- (a) Mesh optimisation (edge swap, node relocation)

At the end : adapted mesh to a prescribed size map

# Motivation III: our choices

Combine:

- simplicity of embedded techniques
- strength of mesh adaptation

Tools:

- level-set description of solid bodies : Sign Distance Function (SDF)
- anisotropic mesh adaptation



Mesh for IBM. Right : Naca0012 airfoil - Left : 2D Complex Ice Shape

# Outline

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Evaluate a mesh

#### Local remeshing

Geometric mesh

Volumic remeshing

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General Ideas Numerical methods Accuracy and mesh adaptation Numerical results Moving bodies (ongoing work)

#### How to locate the objects ?

• Domain does not fit the obstacles

 $\Rightarrow$  need to know where is the inside and the outside

#### Definition: signed distance fonction

Considering a domain  $\Omega_2 \subset \Omega_1$ , delimited by a surface  $\Gamma$ :

$$\phi(x,t) = \begin{cases} d(x,\Gamma) \text{ if } x \in \Omega_1 \setminus \Omega_2 \\ 0 \text{ if } x \in \Gamma \\ -d(x,\Gamma) \text{ if } x \in \Omega_2 \end{cases}$$
(3)



SDF on a mesh for a circle

#### How to impose boundary conditions ?

- With IBM solid wall BCs are taken into account differently
- Penalization : account for the rigid solid (through the governing equations) using a penalty term
  - Idea: extend the velocity field inside the solid



### About accuracy

- Penalty term active inside the solid only
   ⇒ accuracy depends on the capture of the interface
- Our proposition : mesh adaptation to improve accuracy of the SDF



Characteristic function for a circle

# About accuracy

- Penalty term active inside the solid only
  - $\Rightarrow$  accuracy depends on the capture of the interface
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Characteristic function for a circle

### Physical problem

Full compressible Navier-Stokes equations:

$$\left\{ \begin{array}{l} \partial_t \boldsymbol{U} + \partial_{\boldsymbol{x}} \cdot \boldsymbol{\underline{F}} = \partial_{\boldsymbol{x}} \cdot \boldsymbol{\underline{G}} \end{array} \right. \tag{4}$$

$$\boldsymbol{U} = \begin{pmatrix} \rho \\ \rho \boldsymbol{u} \\ \rho e \end{pmatrix}, \quad \underline{\boldsymbol{F}} = \begin{pmatrix} \rho \boldsymbol{u} \\ \rho \boldsymbol{u} \otimes \boldsymbol{u} + p \underline{\mathbf{Id}} \\ (\rho e + p) \boldsymbol{u} \end{pmatrix} \quad \text{and} \quad \underline{\boldsymbol{G}} = \begin{pmatrix} 0 \\ \underline{\boldsymbol{\pi}} \\ \underline{\boldsymbol{\pi}} \boldsymbol{u} + \boldsymbol{q} \end{pmatrix}$$
  
with  $\underline{\boldsymbol{\pi}} = \mu \left( \left[ \frac{\partial \boldsymbol{u}}{\partial \boldsymbol{x}} \right] + \left[ \frac{\partial \boldsymbol{u}}{\partial \boldsymbol{x}} \right]^T - \frac{2}{3} \left[ \frac{\partial}{\partial \boldsymbol{x}} \cdot \boldsymbol{u} \right] \underline{\mathbf{Id}} \right)$  the stress tensor.

#### Boundary conditions:

- inflow/outflow on the outer boundary
- no-slip boundary on the obstacles  $\Gamma_{S^i}$ :

$$\left\{ \begin{array}{l} u_{\Gamma_{S^i}} = v_{\Gamma_{S^i}} = w_{\Gamma_{S^i}} = 0 \\ T_{\Gamma_{S^i}} = cte \end{array} \right.$$



# Residual distribution schemes

overview

 $\bullet~1$  - Compute  $\Phi^T$ 

• 2 - Distribute  $\Phi^T$  to each DoF of the triangle

Nodal Residual

$$\Phi_i^T = \beta_i^T \Phi^T$$



• 3 - Gathering all the contributions of each triangle where i belongs

Residual Scheme

$$\sum_{T \ni i} \Phi_i^T(u_h) = 0$$



#### Resolution of the RDS scheme

• The obtained RDS scheme

$$\sum_{T \ni i} \Phi_i^T = 0$$

• is solved using a pseudo-iterative scheme

$$\begin{cases} \frac{u_i^{n+1} - u_i^n}{\Delta t} + \frac{1}{|C_i|} \sum_{T \ni i} \Phi_i^T = 0\\ u_i^0 \ given \end{cases}$$

- Implicit scheme is used such that  $1/\eta >> 1$ .
- $\eta = 10^{-12}$  in our steady simulations.

# BCs inside penalty methods

- Penalty source term to impose BCs
- Accuracy depends on the capture of the interface
- Our proposition : use mesh adaptation to improve accuracy of the SDF



Characteristic function for a circle

# Mesh adaptation background: metric specification

•  $d \times d$  positive definite symmetric matrix:

$$M = \mathcal{R} \Lambda \mathcal{R}^{-1}$$

 ${\cal R}$  prescribes the orientation of the edges  $\Lambda$  prescribes the size

• Length definition for an edge e:

$$l_M(e) = \int_0^1 \sqrt{e^t M(t)e} \, dt$$

• Metric intersection:

 $M = M_1 \cap M_2$ 



#### Mesh Adaptation : two criteria

Accurate representation of level-set function,



**2** Accurate capture of flow features.

Metric definition for good accuracy of level-set  $_{\tt [Frey and al.]}$ 

- Let's  $\varepsilon$  an error,  $h_{min}$  (resp.  $h_{max}$ ) the minimal (resp. max.) length edge.
- The following metric allows to control the error of an isovalue:

$$M = R \ diag\left(\frac{1}{\varepsilon^2}, \frac{|\lambda_1|}{\varepsilon}, \frac{|\lambda_2|}{\varepsilon}\right) R^T \tag{8}$$

with  $R = (\nabla \Phi, v_1, v_2)$ ,  $(v_1, v_2)$  a basis of the tangent plane to the boundary and  $\lambda_i$  eigenvalues of the Hessian of  $\Phi$ .

- In order to control the 0 isovalue,
  - $\forall$  nodes close to  $\Gamma_S$ , prescribe M
  - $\forall$  other nodes, increase linearly  $h_{min}$  and  $\varepsilon$  until  $h_{max}$ .

# Example of level-set mesh adaptation



• near the 0-level-set :

-hmax 0.06 -hmin 0.005 -eps 0.005

• elsewhere : isotropic mesh

# Example of level-set mesh adaptation



• near the 0-level-set :

-hmax 0.06 -hmin 0.01 -eps0.01

• elsewhere : isotropic mesh

#### Mesh adaptation

Goal : accurate solution with minimum degrees of freedom ( $\Rightarrow$  decreasing CPU time).



# Mesh adaptation with penalization

- Laminar subsonic flow around Naca0012.
- $\bullet~{\rm Reynolds}~5000$  ; Mach 0.5 ; no angle of attack



Initial mesh : embedded (49 000 pts) and fitted (45 000 pts)

Mesh adaptation with penalization: leading and trailing edge

• physical adap parameter:

$$\varepsilon = 5e - 4; h_{min} = .10^{-4}; h_{max} = 2$$

• interface adap parameter:

$$\varepsilon = h_{min} = 10^{-4}; \ h_{max} = 2$$



Adapted mesh : embedded (101 000 pts) and fitted (85 000 pts)

#### Numerical results: Supersonic flow around a triangle <sup>4</sup>



 $h=0.5, \quad \theta=20 \text{ deg}, \quad S=(0.5\,,\,1),$   $Re=5\times 10^4, \quad \text{Prandtl nb}=0.72, \quad M_1=2, \quad T_s=3.$ 

Penalized parameters inside the triangle  $\boldsymbol{u} = 0, T = 3$ 

<sup>&</sup>lt;sup>4</sup>O. Boiron, G. Chiavassa, and R. Donat. *Computers and Fluids*, 2009.

#### Numerical results: Supersonic flow around a triangle

- Initial mesh : 30407 nodes and 60730 triangles
- Interface adaptation parameters :

$$\varepsilon = h_{min} = 1.10^{-4}; h_{max} = 2$$



Numerical results: Supersonic flow around a triangle

- Initial mesh : 30407 nodes and 60730 triangles
- Adaptation parameters :  $\varepsilon = h_{min} = 1.10^{-4}$ ;  $h_{max} = 2$



#### Numerical results: Supersonic flow around a triangle

- Initial mesh : 30407 nodes and 60730 triangles
- Adaptation parameters :  $\varepsilon = h_{min} = 1.10^{-4}$ ;  $h_{max} = 2$
- after 3 cycles of adaptation : 49648 nodes and 99184 triangles



#### Rotation of a rectangular block



0 isoline, from left to right : t = 0, t = 1.64, t = 2.71



#### Rotation of a rectangular block: mass loss

